

Lecture 14: Enthalpy

Enthalpy, C_P , γ , $q_{in} = -q_{out}$, Non-standard enthalpy

Enthalpy

Motivation

- Many chemical processes occur at constant pressure
- Measuring heat is annoying because it is a path function
- What if we could have a state function for constant pressure processes?

Internal energy works for constant volume processes:

$$dU = dq + dw \implies dU = dq_V$$

We define enthalpy to be the constant pressure analog:

Enthalpy

$$H = U + PV$$

$$\Delta H = \Delta U + P\Delta V$$

Change in enthalpy is the heat transferred in a constant pressure process

Enthalpy Derivation

Starting from First Law:

$$\Delta U = q + w$$

Consider constant pressure:

$$\Delta U = q_P - P\Delta V$$

Rearrange:

$$\Delta U + P\Delta V = q_P$$

$$\Delta U + \Delta(PV) = q_P$$

$$\Delta H = \Delta(U + PV) = q_P$$

Heat Capacity

Constant Volume Heat Capacity

$$C_V = \left(\frac{\partial U}{\partial T} \right)_V$$

Constant volume heat capacity

$$dU = dq + dw = dq - PdV$$

At constant volume:

$$dU = dq_V$$

Constant Pressure Heat Capacity

$$C_P = \left(\frac{\partial H}{\partial T} \right)_P$$

Constant pressure heat capacity

$$dH = dU + d(PV)$$

$$dH = dq + dw + PdV + VdP$$

At constant pressure:

$$dH = dq_P$$

Evaluating Heat Capacity

Conceptually: $C_P > C_V$

- Constant Volume - heat increases the internal energy
- Constant Pressure - Volume increases, expansion work, extra energy needed

Mathematical Derivation:

$$H = U + PV$$

Substitute Ideal Gas Law:

$$H = U + nRT$$

Take Partial:

$$\frac{dH}{dT} = \frac{dU}{dT} + nR$$

$$C_P = C_V + nR$$

Relating Heat Capacities

$$\overline{C_P} = \overline{C_V} + R$$

Get $\overline{C_V}$ from equipartition,
always at high T limit

Adiabatic Expansion of Ideal Gas

Another way to relate heat capacities is to use a ratio, recall last lecture:

$$n\overline{C_V}dT = -PdV$$

Substitute ideal gas law $PV = nRT$:

$$n\overline{C_V}dT = -\frac{nRT}{V}dV$$

Group similar terms and integrate:

$$\int_{T_1}^{T_2} \frac{1}{T}dT = -\frac{R}{\overline{C_V}} \int_{V_1}^{V_2} \frac{1}{V}dV$$
$$\ln\left(\frac{T_2}{T_1}\right) = -\frac{R}{\overline{C_V}} \ln\left(\frac{V_2}{V_1}\right)$$

Adiabatic Expansion of Ideal Gas

Define γ :

$$\gamma = \frac{\overline{C_P}}{\overline{C_V}} \quad \overline{C_P} - \overline{C_V} = R$$

Therefore:

$$\frac{R}{\overline{C_V}} = \frac{\overline{C_P} - \overline{C_V}}{\overline{C_V}} = \gamma - 1$$

Substituting back:

$$\ln\left(\frac{T_2}{T_1}\right) = -(\gamma - 1) \ln\left(\frac{V_2}{V_1}\right)$$

$$\boxed{\frac{T_2}{T_1} = \left(\frac{V_1}{V_2}\right)^{\gamma-1}}$$

Conservation of Energy: $q_{in} = -q_{out}$

Conservation of Energy

$$q_{in} = -q_{out}$$

Energy released from one object
gets absorbed by the other

A steel rod (10 g, heat capacity $0.5 \frac{\text{J}}{\text{g}^\circ\text{C}}$) is heated to 75°C . The rod is set on a concrete block (20 g, heat capacity $0.1 \frac{\text{J}}{\text{g}^\circ\text{C}}$) that is at 25°C . When the two materials come to thermal equilibrium, what is their final temperature?

$$q_{\text{steel}} = -q_{\text{concrete}}$$

$$m_{\text{steel}} C_{s,\text{steel}} (T_f - 75^\circ\text{C}) = -m_{\text{concrete}} C_{s,\text{concrete}} (T_f - 25^\circ\text{C})$$

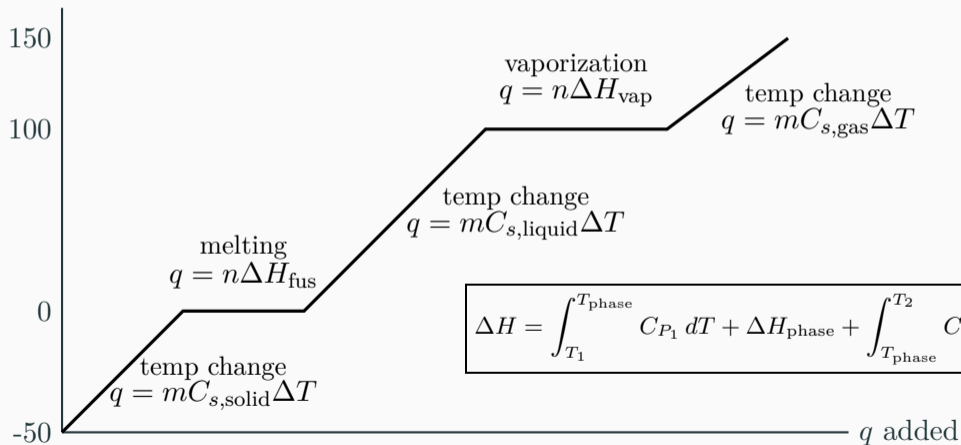
$$10 \text{ g} (0.5 \frac{\text{J}}{\text{g}^\circ\text{C}}) (T_f - 75^\circ\text{C}) = -20 \text{ g} (0.1 \frac{\text{J}}{\text{g}^\circ\text{C}}) (T_f - 25^\circ\text{C})$$

$$5T_f - 375 = -2T_f + 50$$

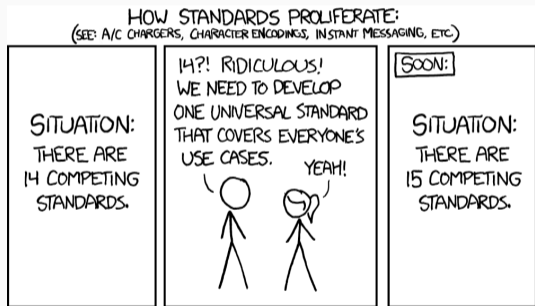
$$T_f = 60.7^\circ\text{C}$$

Heating Curve

Temperature ($^{\circ}\text{C}$)



Standard Conditions



2 Standard Conditions

Thermodynamics

SATP: 298 K, 1 bar or 1 atm

Gases

STP: 273 K, 1 bar or 1 atm

SATP States of Matter

Liquid: Br₂, Hg

Gas: H₂, O₂, N₂, F₂, Cl₂, He, Ne, Ar,
Kr, Xe, Rn

Diatomic: H₂, O₂, N₂, F₂, Cl₂, Br₂, I₂

Otherwise, mono-atomic solid

Non-Standard Enthalpies

Gen Chem: Heat capacities independent of temperature, always use same $\Delta H_{\text{rxn}}^{\circ}$

PChem: Heat capacities can be temperature dependant, calculate ΔH_{rxn} at diff T

Calculating $\Delta H_{\text{rxn}}(T_2)$

For a reaction $aA + bB \rightarrow yY + zZ$

$$\Delta H_{\text{rxn}}(T_2) = \Delta H_{\text{rxn}}(T_1) + \int_{T_1}^{T_2} \Delta C_P(T) dT$$

$$\Delta C_P(T) = yC_{P,Y}(T) + zC_{P,Z}(T) - aC_{P,A}(T) - bC_{P,B}(T)$$

Example: Non-Standard Enthalpies

Given NH_3 $\Delta H_f^\circ = -46.11 \text{ kJ/mol}$, determine NH_3 $\Delta H_f(1000 \text{ K})$

$$\frac{1}{2} \text{N}_2 + \frac{3}{2} \text{H}_2 \longrightarrow \text{NH}_3$$
$$C_P^\circ(\text{H}_2)/\frac{\text{J}}{\text{K}\cdot\text{mol}} = 29.07 - 0.837 \times 10^{-3}T + 2.012 \times 10^{-6}T^2$$
$$C_P^\circ(\text{N}_2)/\frac{\text{J}}{\text{K}\cdot\text{mol}} = 26.98 + 5.912 \times 10^{-3}T - 0.3376 \times 10^{-6}T^2$$
$$C_P^\circ(\text{NH}_3)/\frac{\text{J}}{\text{K}\cdot\text{mol}} = 25.89 + 32.58 \times 10^{-3}T - 3.046 \times 10^{-6}T^2$$

$$\Delta H_f^\circ(1000 \text{ K}) = \Delta H_f^\circ(298 \text{ K}) + \int_{298 \text{ K}}^{1000 \text{ K}} \Delta C_P^\circ(T) dT$$

$$\Delta C_P^\circ(T)/\frac{\text{J}}{\text{K}\cdot\text{mol}} = C_P^\circ(\text{NH}_3) - \frac{1}{2}C_P^\circ(\text{N}_2) - \frac{3}{2}C_P^\circ(\text{H}_2)$$
$$= -31.21 + 30.88 \times 10^{-3}T - 5.895 \times 10^{-6}T^2$$

$$\int_{298 \text{ K}}^{1000 \text{ K}} \left[-31.21 + 30.88 \times 10^{-3}T - 5.895 \times 10^{-6}T^2 \right] dT$$

$$= (-21.91 + 14.07 - 1.913) \text{ kJ/mol}$$

$$= -9.75 \text{ kJ/mol} \implies \Delta H_f(1000 \text{ K}) = \boxed{-55.86 \text{ kJ/mol}}$$